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← NOTE: date shift due to snow cancellation on 2/8

Ampère's Law (cont)

□ Similar in spirit to Gauss' Law to determine \vec{E} , this rule allows us to exploit symmetries to find \vec{B}

$$\sum_{\text{closed path}} B_{\parallel} \Delta L = \mu_0 I_{\text{enclosed}} \quad (\text{Giordano version})$$

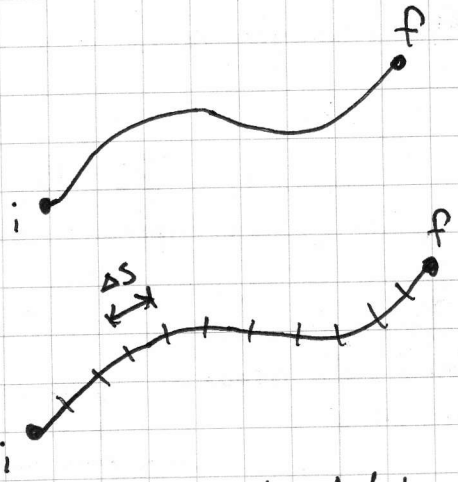
We can alternatively write this as:

$$\oint_C \vec{B} \cdot d\vec{s} = \mu_0 I_{\text{enclosed}} \quad \left(\begin{array}{l} \text{NOTE} \\ I_{\text{enclosed}} = I_{\text{through}} \end{array} \right)$$

here \oint indicates a 'line integral' (line integration is performed around a closed curve). The integrand dot product is a scalar that represents a specific relationship between \vec{B} and the curve of interest.

Math Aside (re line integrals)

- Consider an arbitrary line (that doesn't cross itself) stretched between i and f (two points)
- chop that line up into little segments of length Δs
- the length of the line is then



$$L = \sum_k \Delta s_k \rightarrow \int_i^f ds$$

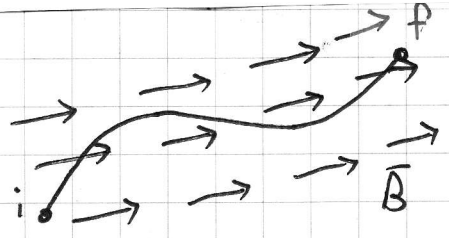
→ curve has total length L

where $dS = \lim_{\Delta S \rightarrow 0} \Delta S$

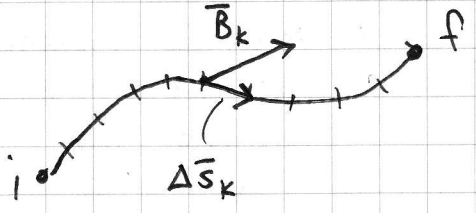
• this last piece is what is called a line integral, i.e. we chopped the line up into infinitely many infinitesimal pieces, then added them up

ex) $\int_a^b dx = x|_a^b = b-a$ is just a line integral along the x-axis from b to a!

□ Now what happens if we make things a bit more interesting and consider our line relative to a magnetic field \vec{B} ?



• the k'th element along the line has length ΔS , but also has a direction associated with it (tangent to the line), the $\Delta \vec{S}_k$ is a vector



• we can also consider the magnetic field at that point (\vec{B}_k) which is also a vector

• Suppose we want to compute the dot product $\vec{B}_k \cdot \Delta \vec{S}_k$ at each segment and then add them up along the line (this is what we need to do for Ampère's Law!), then we have:

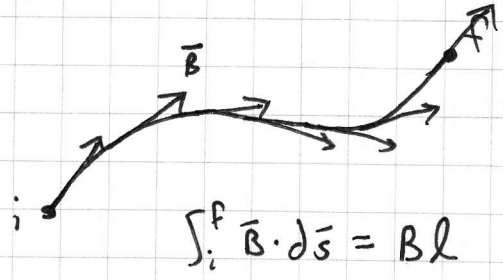
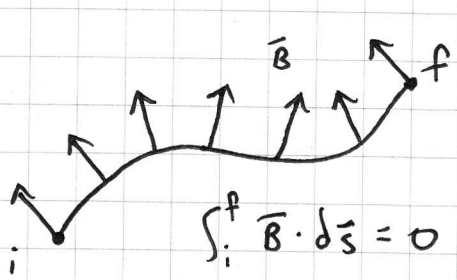
$$\sum_k \vec{B}_k \cdot \Delta \vec{S}_k \rightarrow \int_i^f \vec{B} \cdot d\vec{S} = \text{line integral of } \vec{B} \text{ from } i \text{ to } f$$

• If we make use of symmetry, this calculation is easy:
 - if \vec{B} is perpendicular everywhere to the line, $\vec{B} \cdot d\vec{S} = 0$ and integral is zero
 - if \vec{B} is parallel (i.e. tangent) to the curve everywhere and B is const. along the line, then (cont. \checkmark)

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(cont.) $\vec{B} \cdot d\vec{s} = B ds$ and $\int_i^f \vec{B} \cdot d\vec{s} = B \int_i^f ds = BL$

→ we can also show this visually



□ Now back to Ampère's Law: $\oint_c \vec{B} \cdot d\vec{s} = \mu_0 I_{\text{enclosed}}$

- $\oint \vec{B} \cdot d\vec{s}$ indicates our curve is a 'closed' one (i.e. the starting point and ending point are the same); put another way, we integrate around a loop
- I_{enclosed} is the total current passing through the surface that the closed curve enclosed
(Aside: sometimes I_{enclosed} is written as

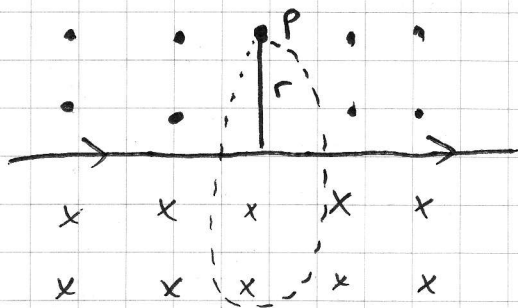
$I_{\text{enclosed}} = \iint_S \vec{J} \cdot d\vec{s}$ where \vec{J} is the 'current density' and \iint_S indicates integrating over the surface S that is enclosed by c ; Gauss' Law is written in a similar fashion in its general form

- Like Gauss' Law, $\oint_c \vec{B} \cdot d\vec{s} = \mu_0 I$ has the following properties:
- the integral is independent of the shape around the current
 - its independent of where the current passes through
 - depends only upon the total amount of current passing through the integration paths enclosing area

→ For \mathcal{H} lo, for this to be generally useful, we need to apply it to case where we can find a path along which B is const. (these are few and far between!)

ex a straight wire w/ current I

◦ path is a circle of radius r around the wire
(\vec{B} is const. along this circle!)



$$\oint_C \vec{B} \cdot d\vec{s} = B \oint_C ds$$

$$= B (2\pi r) = \mu_0 I$$

$$\rightarrow \boxed{B = \frac{\mu_0 I}{2\pi r}}$$

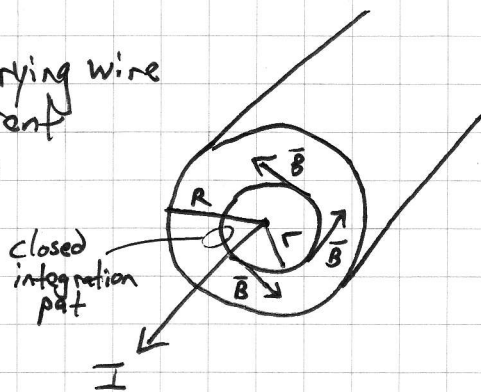
◦ as shown in ch. 20.7 by Giordano, for a 1 A current, 1 cm away from the wire yields:

$$B = \frac{(4\pi \times 10^{-7} \text{ T}\cdot\text{m/A})(1 \text{ A})}{2\pi (0.01 \text{ m})} = 2 \times 10^{-5} \text{ T}$$

→ 1 A is a large current and 0.01 m is pretty close to the wire, yet the field strength is quite small!
(not even $\frac{1}{2}$ that of earth)

ex Magnetic field inside a current-carrying wire of radius R . Assume the current density (J) is uniform over the cross-section of the wire.

◦ make use of circular symmetry!
(see right)



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ex. (cont.)

- Consider a circle of radius r ($r < R$). The current passing through is:

$$I_{\text{through}} = JA = J\pi r^2$$

- We assumed the current density is uniform, so we can determine J in terms of I and R :

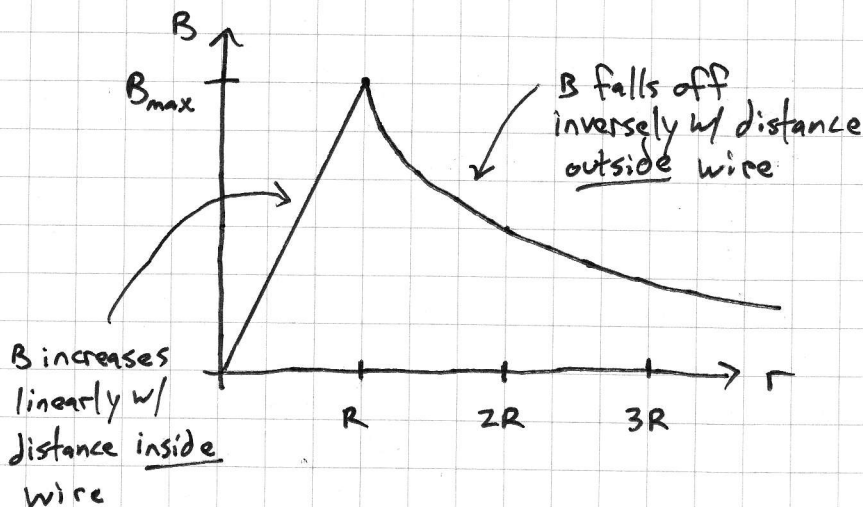
$$J = \frac{I}{A} = \frac{I}{\pi R^2} \rightarrow I_{\text{through}} = \frac{r^2}{R^2} I$$

- Now \vec{B} is uniform and tangent to our circle, so we have:

$$\oint \vec{B} \cdot d\vec{s} = B 2\pi r = \mu_0 I_{\text{through}} = \mu_0 \left(\frac{r^2}{R^2} \right) I$$

- Now we can solve for B :

$$B = \frac{\mu_0 I}{2\pi R^2} r$$



$$B_{\text{max}} = \frac{\mu_0 I}{2\pi R}$$

(i.e. B is largest on the surface of the wire)

□ Finding B for a loop of coil is trickier and beyond the scope of 1410. We will simply state the conclusion (as well as that for a coil of N loops) and provide the derivation via the Biot-Savart law below for reference (you won't be responsible for this, for an exam) [you do need to know the two directly below though!]

• Single ~~coil~~ ^{loop} of wire w/ current I :
(radius R , at center of loop)

$$B_{\text{loop}} = \frac{\mu_0 I}{2R}$$

• coil of N loops of radius R w/ current I (at center of coil) :

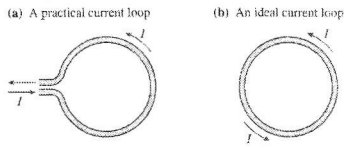
$$B_{\text{coil}} = N \frac{\mu_0 I}{2R}$$

(they simply sum up together!)

The magnetic field of a current loop

FIGURE 32.16a Shows a current loop, a circular loop of wire with radius R that carries current I . Find the magnetic field of the current loop at distance z on the axis of the loop.

FIGURE 32.16 A current loop.

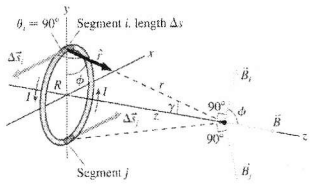


The direction of \vec{B}_i , the magnetic field due to the current in segment i , is given by the cross product $\Delta\vec{s}_i \times \hat{r}$. \vec{B}_i must be perpendicular to $\Delta\vec{s}_i$ and perpendicular to \hat{r} . You should convince yourself that \vec{B}_i in Figure 32.17 points in the correct direction. Notice that the y -component of \vec{B}_i is canceled by the y -component of magnetic field \vec{B}_j due to the current segment at the bottom of the loop, 180° away. In fact, every current segment on the loop can be paired with a segment 180° away, on the opposite side of the loop, such that the x - and y -components of \vec{B} cancel and the components of \vec{B} parallel to the z -axis add. In other words, the symmetry of the loop requires the on-axis magnetic field to point along the z -axis. Knowing that we need to sum only the z -components will simplify our calculation.

Real coils need wires to bring the current in and out, but we'll model the coil as a current moving around the full circle shown in FIGURE 32.16b.

FIGURE 32.17 shows a loop for which we've assumed that the current is circulating ccw. We've chosen a coordinate system in which the loop lies at $z = 0$ in the xy -plane. Let segment i be the segment at the top of the loop. Vector $\Delta\vec{s}_i$ is parallel to the x -axis and unit vector \hat{r} is in the yz -plane, thus angle θ_i , the angle between $\Delta\vec{s}_i$ and \hat{r} , is 90° .

FIGURE 32.17 Calculating the magnetic field of a current loop.



We can use the Biot-Savart law to find the z -component $(B_i)_z = B_i \cos \phi$ of the magnetic field of segment i . The cross product $\Delta\vec{s}_i \times \hat{r}$ has magnitude $(\Delta s)(1) \sin 90^\circ = \Delta s$, thus

$$(B_i)_z = \frac{\mu_0 I \Delta s}{4\pi r^2} \cos \phi = \frac{\mu_0 I \cos \phi}{4\pi(z^2 + R^2)^{3/2}} \Delta s$$

where we used $r = (z^2 + R^2)^{1/2}$. You can see, because $\phi + \gamma = 90^\circ$, that angle ϕ is also the angle between \hat{r} and the radius of the loop. Hence $\cos \phi = R/r$, and

$$(B_i)_z = \frac{\mu_0 I R}{4\pi(z^2 + R^2)^{3/2}} \Delta s$$

The final step is to sum the magnetic fields due to all the segments:

$$B_{\text{loop}} = \sum_i (B_i)_z = \frac{\mu_0 I R}{4\pi(z^2 + R^2)^{3/2}} \sum_i \Delta s$$

In this case, unlike the straight wire, none of the terms multiplying Δs depends on the position of segment i , so all these terms can be factored out of the summation. We're left with a summation that adds up the lengths of all the small segments. But this is just the total length of the wire, which is the circumference $2\pi R$. Thus the on-axis magnetic field of a current loop is

$$B_{\text{loop}} = \frac{\mu_0 I R}{4\pi(z^2 + R^2)^{3/2}} 2\pi R = \frac{\mu_0 I R^2}{2(z^2 + R^2)^{3/2}}$$

Note that at the center of the coil, $z=0$ and the general expression reduces to B_{loop}

from Knight